10.37 Chemical and Biological Reaction Engineering, Spring 2007 Prof. William H. Green Lecture 2: The Reaction Rate & Reaction Mechanisms

The lecture covers: Definitions in terms of reacting compounds and reaction extent, rate laws, Arrhenius equation, elementary, reversible, non-elementary, catalytic reactions.

From previous lecture:

$$\frac{dN_A}{dt} = F_{Ao} - F_A + G_A, \ G_A = \int r_A dV$$

Example:

 $A + B \rightarrow 2C$ *Reactions are reversible (often will neglect reverse)

$$X_{A} = \frac{N_{Ao} - N_{A}}{N_{Ao}} \qquad X_{A} = \frac{F_{Ao} - F_{A}}{F_{Ao}} \qquad X_{C} = \frac{F_{C}}{2F_{Ao}}$$
$$\underbrace{A,B}_{F_{Ao}} \qquad \underbrace{C,A,B}_{F_{Bo}}$$

Figure 1. A reactor with reactants A and B constantly flowing in and product C and unused reactants A and B flowing out.

$$F_{Ao} = \frac{\text{moles A flowing in}}{\text{sec}} = [A]_{input} \underbrace{v_{in}}_{\frac{\text{liters}}{\text{sec}}} = [A]_{o} v_{o}$$

$$F_{A} = \frac{\text{moles A flowing out}}{\text{sec}} = [A]_{output} v_{out}$$

$$X = 1 - \frac{[A]_{output} v_{out}}{[A]_{in} v_{in}}$$

Closed reactor, const. V

Detailed balance- all steps in equilibrium, total system

$$\frac{d[A]}{dt} = r_A = -k[A][B]$$

$$K_{eq} = \frac{[C]^2}{[A][B]}$$
when $[A][B] = \frac{[C]^2}{K_{eq}}$ the rxn. stops -> r_A=0

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$$r_{A} = -k \left[[A] [B] - \frac{[C]^{2}}{K_{eq}} \right], \quad k_{rev} = \frac{k_{for}}{K_{eq}}, \text{ forward-reverse in one expression}$$

Catalysis

$$r_{A, forward} = k_{cat} \left[\text{catalyst} \right] \left[A \right] \underbrace{f\left(\begin{bmatrix} B \end{bmatrix} \right)}_{\text{may be included}}_{i.e. \text{ when B is very small}}$$

Rate limiting step determines the kinetics (slow step). The kinetics are insensitive to [B] because B is not part of this slow step.

$$r_{A,reverse} = r_{A,forward} \frac{\left[C\right]^{2}}{K_{eq}\left[A\right]\left[B\right]}$$

$$r_{A,net} = -k_{cat} \left[\text{catalyst}\right] \left(\left[A\right] - \frac{\left[C\right]^{2}}{K_{eq}\left[A\right]\left[B\right]}\right)$$

$$K_{eq} = e^{-\Delta G/RT} \qquad \Delta G = \Delta G_{f,products}^{o} - \Delta G_{f,reactants}^{o}$$
Standard state

$$A \to B + C$$

$$K_{\not \bowtie} = \frac{[B][C]}{[A]} [=] \frac{\text{moles}}{\text{liter}}$$

$$K_{C}$$

Partial Pressures

$$\frac{p_B p_C}{p_A P^o} = K_{eq} = \frac{[B][C]}{[A]\frac{P^o}{RT}}$$

Ideal Gas: $pV = nRT \Rightarrow \frac{n}{V} = \frac{P}{RT}$

 P° is the standard state pressure (1 atm), this makes the units cancel. Using partial pressures is accurate within 10%, more error with liquids.

Stoichiometric coefficient

$$N_{A} = N_{A,initial} + \sum_{i} v_{A,i} \xi_{i}$$

Extent of rxn.

 $N_{C} = N_{C,initial} + \sum_{i=1}^{N_{ran}} v_{C,i} \xi_{i}$

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Reaction trajectory-Plot state of system $\xi = N_{Ao}$ t = 10 ξ t = 0.01 $\frac{d}{dt}(\underline{N}) = \underline{F}(\underline{N})$



Conservation Laws

Conserve atoms $2CH_4 + O_2 \rightarrow C_2H_4 + 2H_2O$ $\underbrace{C_A}_{\text{constant moles}} + C_BN_B + C_CN_C = \text{const.}$ $\underline{C} : 1 \times N_{CH_4} + 2 \times N_{C_2H_4} = N_{C,\text{initial}}$ $\underline{H} : 4 \times N_{CH_4} + 4 \times N_{C_2H_4} + 2N_{H_2O} = N_{H,\text{initial}}$

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